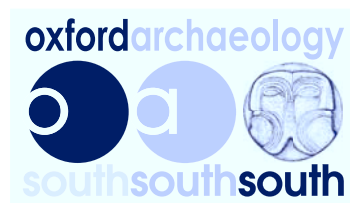


# Godley Bridge Survey Surrey



## Archaeological Monitoring of Seismic Ground Testing



August 2010

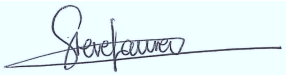
**Client: Tesla - IMC  
International Limited**

Issue No: 1  
OA Job No: 4769  
NGR: SU 93450 37670  
and SU 93142 36096





Client Name: Tesla-IMC International Limited  
Client Ref No: 108450  
Document Title: Godley Bridge Survey, Surrey. Archaeological Monitoring of Seismic Ground Testing  
Document Type: Evaluation Report  
Issue Number: 1  
Grid Reference: SU 93450 37670 and SU 93142 36096  
Planning Reference:  
OA Job Number: 4769  
Site Code: CHGOB 10  
Invoice Code: CHGOBEV  
Receiving Museum: TBC  
Museum Accession No: N/A  
Event No: N/A

Issue	Prepared by	Checked by	Approved by	Signature
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Document File Location \CHGOBEV\_Godley\_Bridge\_Surrey\002Reports  
Graphics File Location \\Servergo\invoice codes a thru h\C\_invoice codes\CHGOBEV  
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## Godley Bridge Survey, Surrey

### Archaeological Monitoring of Seismic Ground Testing

*Archaeological Evaluation Report*

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## Summary

*On 26th May 2010 Oxford Archaeology undertook a field impact assessment of geotechnical seismic survey investigations upon the potential archaeological resource at two trial locations north-east of Haslemere, Surrey. The investigation was undertaken in advance of, and to inform, a programme of geotechnical prospecting within the surrounding landscape.*

*The survey utilised a 200g explosive charge buried 2 m deep into the underlying sediments. Controlled archaeological excavation and sampling of the discharged explosive at two locations established that these had a localised impact upon the surrounding sediment and that this was unlikely to significantly affect any archaeological remains. The explosive force created blast craters with diameters of c 0.65 m surrounded by areas of sediment compaction. The localised outcrops of ironstone found within the Weald Clay Formation were found to be resilient to the impacts of the blast.*



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## 1 INTRODUCTION

### 1.1 Location and scope of work

1.1.1 Oxford Archaeology South (OAS) was commissioned by TESLA - IMC International Ltd to undertake archaeological recording of the impact of geotechnical prospecting (seismic survey) at two trial locations north-east of Haslemere, Surrey (Figure 1). The County Archaeologist for Surrey County Council requested that the potential impacts of these works be assessed ahead of the full survey of the surrounding landscape (Figure 2). The fieldwork was undertaken on 26th May 2010.

### 1.2 Previous archaeological testing

1.2.1 Very little data is currently available detailing the potential impacts of seismic testing upon buried archaeological resources. However, a similar study has been recently undertaken near to Oldbury-upon-Severn Power Station, South Gloucestershire, by OAS and IMC Geophysics (OA 2009). This assessed the impact of this technique on the important prehistoric peat and alluvial deposits within the Severn levels area. This study utilised a 50g explosive charge buried at a depth of 2 m into the underlying soft sediments. Excavation and sampling of two discharged survey locations at Oldbury established that this method had a very localised impact upon the surrounding sediment and that was unlikely to significantly affect archaeological remains. The blasts created a c 0.35 m crater and an additional 50 mm zone of sediment liquefaction and 'compaction' around the crater.

1.2.2 No archaeological data is currently available for the impact of seismic testing upon firm or hard sediments or the affect upon buried archaeological structures.

### 1.3 Geology and topography

1.3.1 The trial pits were excavated within the mudstone and sandstone elements of the Weald Clay Formation.

## 2 EVALUATION AIMS AND METHODOLOGY

### 2.1 Aims

2.1.1 The purpose of this investigation was to assess the impact of the seismic survey upon the surrounding sediments and interpret how this may affect potential archaeological deposits. The trial pits were designed to assess the impact of the blast and resulting shock wave by recording any resultant sediment distortion or compaction.

### 2.2 Methodology

2.2.1 Two trial locations (NGR SU 93450 37670 and SU 93142 36096) were subject to seismic testing using buried explosive charges to investigate the sediments and underlying geology. The seismic survey was undertaken using 200g charges inserted into the ground at the bottom of a 50 mm diameter and 2 m deep hole excavated with a spiral auger (Plates 1 and 3). These were backfilled with 10 mm pea gravel prior to each discharge. The locations were recorded as latitude and longitude with a hand-held GPS instrument with an accuracy of  $\pm 10$  m and subsequently converted to OSGB36.

2.2.2 Following the explosive discharge and data capture for the survey, both locations were machine excavated under archaeological supervision. The surface dimensions of the





trial pits were c 1.5 m by 3.5 m and up to 2.50 m deep to reveal the charge detonation impact crater (at between 1.75 and 2 m below ground level). The trial pits were excavated in controlled spits using a mechanical excavator initially fitted with a toothless bucket and under the direct supervision of an experienced geoarchaeologist. The auger hole used to plant the charge was maintained within the section along one side of the trench. At the point when stiff geological deposits were encountered and after the absence of archaeological deposits had been established, machine excavation continued to the required depth with a toothed bucket. It proved to be impractical to safely shore the trenches with the equipment available. As a result all recording of the trial pits deeper than 1 m was completed by observation and measurement from the surface and detailed analysis of the sediments was undertaken as they were excavated and brought to the surface by the machine. Recording of the sediments was undertaken by a qualified geoarchaeological specialist.

### 3 RESULTS

#### 3.1 Description of deposits

- 3.1.1 The trial pits revealed a sequence of laterally equivalent geological deposits of the Weald Clay Formation. No evidence of more recent (Holocene) soil formations, archaeological deposits or artefacts was encountered during the excavation of the trial pits.
- 3.1.2 The trial pits were excavated to a depth of 2.20-2.40 m BGL encountering a loose light reddish yellow layered coarse sand with frequent ironstone inclusions from 1.30 m BGL (101 and 201). The ironstone formed distinct bands within the natural bedrock. A second deposit of similar soft light brownish yellow sandy and silty clay (102 and 202) was identified overlying this between 0.30 m and 1.30 m BGL. A 0.30 m thick layer of weathered and parched friable sandy/silty clay (103 and 203) overlay this forming the current agricultural ploughsoil within each field. The diffuse boundary between the bedrock and ploughsoils suggests that ploughing has an active contact with the surface of the underlying geological deposits. No evidence for any buried ploughsoils, colluvial or alluvial deposits was identified between the ploughsoil and bedrock.

#### 3.2 Archaeological impact of the seismic testing

- 3.2.1 The discharge of the explosive created a roughly circular blast crater within Test Pit 1 with a diameter of 0.60-0.70 m (Plate 2). The crater was partly filled with the pea gravel backfill from the auger hole that had fallen into the cavity after the explosive had been discharged. A white vapour was also observed to have been released upon the initial excavation of the blast crater. The loose sand surrounding the explosive appears to have been compressed around the blast although no visible signs of sediment distortion, compaction or fracture were identified within the surrounding sand/sandy clay or wider trench sequence. The firm and loose qualities of the ironstone fragments and sand appears to have been effective at limiting and containing the impacts of the blast.
- 3.2.2 The results of Test Pit 2 were very similar, but with the one notable difference that the blast crater was not circular but had a horizontal tear drop-shaped profile (Plate 4). The presence of ironstone towards the east of the charge appears to have been effective at containing and reflecting the blast. The crater measured 0.65 m wide at its greatest by 0.35 m at the centre of the charge detonation. The lumps of ironstone surrounding the blast crater showed only limited signs of blast damage. Again, no visible signs of



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sediment distortion or compaction were observed in the trial pit section beyond the immediate crater area.

## 4 CONCLUSIONS

### 4.1 Potential impacts

4.1.1 The propagation of seismic waves through sediments at a very low strain level (less than 3-10 percent) does not appear to have had a significant affect upon the buried stratigraphy. It is also reasonable to suggest that the containment of the blast to a localised area within less than 1 m of the detonation location makes it unlikely that potential buried structures would also be damaged by this level of survey. The waves dissipate with distance and depth from the source, and the level of strain placed upon a rigid structure buried at depth is not likely to be significant. The water and clay mineral content of the sediments will also determine how the seismic wave travels through the sediments. The very localised impact observed during this investigation suggests that archaeological features and deposits are unlikely to be affected by the seismic testing unless they are located within the actual impact area of the explosive blast and resultant crater. The excavation demonstrates that the impacts of the seismic testing are likely to be very localised to within a maximum of between 0.35-0.75 m radius of the blast within the type of geology encountered. Greater localised impacts would be expected within softer sediments with the same explosive charge size. However, the wider survey has been undertaken almost exclusively within the Weald Clay Formation or partly within geologies with similar properties (i.e. Hythe Formation or the Atherfield Clay Formation of Sandstone and Mudstone). The wider survey area is presented in Figures 2-5. Detailed locations and ground level elevations are recorded for each test shot location within Appendix B.



## APPENDIX A. TRENCH DESCRIPTIONS AND CONTEXT INVENTORY

Trail Pit 1 (A)				
<b>General description</b>			<b>Orientation</b>	E-W
No archaeological remains. Ploughsoil directly overlying Weald Clay Formation. 200g charge created an evenly distributed crater with a diameter of c. 0.65 m.			<b>Excavation Depth (m)</b>	2.5
			<b>Width (m)</b>	1.5
			<b>Length (m)</b>	3.5
Contexts				
context no	type	Width (m)	Depth BGL (m)	comment
101	Layer	-	1.30-2.50	Loose-soft light reddish yellow sand with freq. well stratified ironstone bands.
102	Layer	-	0.30-1.30	Firm-soft light brownish yellow structureless silty clay/sandy clay with freq. angular ironstone inclusions and silty lenses.
103	Layer	-	0-0.30	Ploughsoil

Trail Pit 2 (B)				
<b>General description</b>			<b>Orientation</b>	E-W
No archaeological remains. Ploughsoil directly overlying Weald Clay Formation. 200g charge created a horizontal tear drop-shaped crater caused by differing planes of resistance within the localised stratigraphy of the geology.			<b>Avg. depth (m)</b>	3.5
			<b>Width (m)</b>	1.5
			<b>Length (m)</b>	2
Contexts				
context no	type	Width (m)	Depth BGL (m)	comment
201	Layer	-	1.30-2.20	Loose light reddish yellow coarse sand with freq. well stratified ironstone bands.
202	Layer	-	0.30-1.30	Soft light yellow structureless silty/sandy clay with freq. ironstone inclusions.
203	Layer	-	0-0.30	Ploughsoil



## APPENDIX B. SURVEY SHOT LOCATIONS

Geodetic Datum: GRS1980

Vertical Datum: NEWLYN

Projection: OSGB36

Recorded elevations are at ground level with all detonations at 2m BGL.

LINE-SHOT#	EASTING	NORTHING	ELEVATION
1-101	490097.67	136576.15	178.440
1-102	490118.63	136580.98	176.336
1-103	490139.84	136590.56	175.327
1-104	490166.60	136601.79	174.492
1-105	490188.66	136602.85	173.257
1-106	490212.55	136596.24	172.229
1-107	490225.31	136592.39	173.473
1-108	490259.31	136620.30	166.927
1-109	490252.56	136644.61	163.739
1-110	490273.23	136664.56	161.914
1-111	490278.03	136674.31	160.280
1-115	490362.67	136742.13	149.023
1-116	490386.91	136746.60	147.744
1-117	490411.21	136751.99	146.663
1-118	490435.96	136756.82	145.345
1-119	490460.32	136760.11	143.798
1-120	490485.02	136765.67	142.146
1-121	490509.01	136774.20	140.841
1-122	490532.53	136783.72	139.494
1-123	490552.10	136796.78	138.663
1-124	490570.93	136814.18	138.254
1-125	490588.68	136831.59	137.965
1-126	490608.64	136845.46	137.890
1-127	490632.07	136849.28	138.155
1-128	490656.32	136844.35	138.572
1-129	490679.97	136837.24	139.138
1-130	490706.37	136833.69	139.501
1-131	490730.66	136842.58	139.741
1-132	490745.89	136861.02	140.226
1-133	490762.58	136848.81	139.326
1-134	490809.94	136832.88	138.093
1-135	490821.82	136828.87	137.623
1-136	490845.49	136820.90	136.377
1-137	490869.20	136812.95	135.211
1-138	490892.92	136804.97	134.257
1-139	490916.59	136797.01	133.526
1-141	490963.97	136781.07	130.371
1-143	491011.40	136765.11	125.111
1-145	491058.77	136749.18	120.106
1-147	491106.18	136733.24	116.539
1-148	491118.02	136729.26	115.681
1-152	491218.96	136674.96	111.155
1-153	491226.08	136664.67	110.976
1-155	491255.19	136623.96	110.370
1-157	491284.26	136583.20	110.324
1-158	491298.83	136562.88	109.973
1-159	491313.46	136542.61	109.068
1-164	491401.70	136455.89	108.231
1-165	491419.09	136437.05	108.680
1-167	491452.70	136398.99	109.726
1-168	491468.71	136381.69	109.571
1-171	491530.36	136383.73	107.880
1-173	491564.53	136399.07	106.559
1-175	491624.78	136411.03	104.923
1-177	491674.48	136407.44	104.462
1-179	491724.60	136406.12	104.306
1-181	491761.87	136402.93	104.696
1-183	491815.26	136370.60	105.865



LINE-SHOT#	EASTING	NORTHING	ELEVATION
1-185	491854.68	136339.88	106.800
1-187	491894.62	136309.18	107.538
1-188	491921.07	136314.04	106.629
1-190	491956.84	136338.26	104.109
1-192	492005.75	136364.70	102.144
1-195	492077.33	136349.63	99.420
1-196	492091.36	136370.40	98.470
1-198	492119.59	136411.77	97.554
1-200	492140.86	136456.85	96.392
1-201	492144.24	136468.90	96.136
1-202	492150.68	136493.14	95.686
1-208	492283.11	136540.52	99.820
1-209	492298.55	136537.57	100.664
1-210	492319.05	136551.99	100.487
1-213	492390.06	136599.70	99.407
1-215	492432.61	136625.93	98.475
1-217	492485.81	136658.72	96.493
1-219	492517.75	136678.41	94.977
1-220	492539.03	136691.52	94.609
1-221	492560.29	136704.63	94.251
1-222	492581.59	136717.76	93.654
1-223	492602.86	136730.86	92.716
1-224	492624.16	136743.98	91.140
1-225	492645.43	136757.08	89.158
1-226	492666.72	136770.22	88.860
1-227	492687.99	136783.34	88.764
1-228	492709.29	136796.45	88.296
1-229	492730.57	136809.58	87.656
1-230	492751.86	136822.69	87.201
1-231	492773.14	136835.79	87.009
1-232	492794.41	136848.92	87.617
1-233	492815.72	136862.04	88.173
1-234	492826.32	136868.58	88.500
1-240	492970.65	137002.14	85.293
1-241	492991.62	136999.63	85.341
1-242	493014.94	136996.48	85.375
1-247	493147.42	136960.38	84.514
1-248	493159.94	136960.07	83.950
1-249	493184.65	136957.03	83.060
1-250	493209.39	136953.34	82.235
1-251	493233.52	136946.71	81.724
1-252	493244.95	136941.87	81.512
1-257	493366.81	136863.45	75.557
1-259	493400.65	136859.48	80.101
1-260	493411.72	136866.67	79.791
1-261	493428.76	136884.66	78.994
1-263	493471.72	136928.85	77.782
1-264	493490.43	136946.06	77.460
1-265	493499.57	136954.21	77.044
1-266	493527.29	136978.16	76.645
1-267	493546.84	136994.79	76.182
1-268	493556.40	137003.26	75.888
1-269	493586.02	137027.76	75.761
1-270	493612.56	137053.00	75.435
1-271	493621.29	137062.42	75.064
1-272	493629.25	137071.29	74.880
1-273	493650.70	137081.80	74.327
1-274	493685.39	137068.19	74.345
1-275	493705.99	137054.01	75.244
1-276	493725.80	137038.74	75.823
1-277	493734.04	137032.65	76.041
1-301	495050.63	136668.83	56.041
1-302	495062.51	136665.76	57.102
1-303	495086.39	136653.88	58.492
1-304	495109.83	136646.99	61.084
1-305	495133.77	136639.95	62.858
1-306	495158.44	136637.83	64.085
1-307	495182.43	136634.24	65.426
1-308	495203.13	136649.61	66.101
1-309	495221.60	136666.45	66.978
1-310	495239.59	136679.55	67.709



LINE-SHOT#	EASTING	NORTHING	ELEVATION
1-311	495264.91	136692.02	67.724
1-312	495275.40	136696.61	67.443
1-313	495277.86	136780.18	50.591
1-314	495301.91	136784.17	50.242
1-315	495323.56	136782.91	50.066
1-316	495348.73	136775.92	50.192
1-317	495371.07	136782.69	49.967
1-318	495395.11	136775.59	50.162
1-319	495422.71	136772.14	51.006
1-320	495445.72	136758.90	49.973
1-321	495456.09	136754.70	49.622
1-322	495481.63	136729.48	49.155
1-323	495499.04	136704.99	49.201
1-324	495514.26	136692.00	49.248
1-325	495547.15	136675.72	49.264
1-326	495559.11	136674.70	49.277
1-327	495583.36	136674.19	49.171
1-328	495608.41	136680.26	49.093
1-329	495556.35	136595.54	65.702
1-330	495580.43	136596.86	66.834
1-333	495672.85	136603.95	67.319
1-335	495720.58	136615.42	67.809
1-337	495761.69	136644.06	67.034
1-339	495798.46	136679.02	65.304
1-341	495833.76	136703.17	64.686
1-343	495873.62	136684.07	64.153
1-345	495909.75	136694.44	63.030
1-347	495942.72	136655.45	63.236
1-349	495987.43	136635.52	61.215
1-350	496012.30	136635.94	58.899
1-351	496035.88	136634.66	56.029
1-353	496082.76	136598.79	49.139
1-355	496110.11	136572.10	47.814
1-356	496128.02	136554.44	46.264
1-359	496181.73	136502.07	45.666
1-360	496199.82	136485.70	45.700
1-362	496232.83	136441.23	45.612
1-364	496281.63	136467.88	45.402
1-365	496303.09	136474.56	45.351
1-366	496329.41	136480.38	45.482
1-367	496349.68	136492.30	45.282
1-381	496620.85	136307.07	49.086
1-382	496632.52	136290.94	49.210
1-383	496657.76	136286.44	50.165
1-384	496682.64	136279.80	50.420
1-385	496708.27	136275.03	50.975
1-386	496737.11	136277.29	52.140
1-387	496759.99	136284.96	53.812
1-388	496774.82	136292.29	55.293
1-394	496938.45	136271.57	67.940
1-395	496950.01	136267.83	68.895
1-396	496971.16	136254.02	70.939
1-397	496991.63	136239.65	72.889
1-398	497010.81	136224.30	72.248
1-399	497031.01	136208.32	70.541
1-400	497050.35	136193.68	68.335
1-401	497070.33	136177.44	65.920
1-402	497088.06	136159.76	63.524
1-403	497104.08	136142.04	62.132
1-404	497118.10	136120.67	61.181
1-405	497129.78	136098.79	60.612
1-406	497137.69	136074.64	60.429
1-407	497144.57	136065.33	60.188
1-411	497255.88	136114.71	56.657
1-412	497266.96	136119.37	56.370
1-413	497290.32	136128.11	55.760
1-415	497338.08	136141.82	54.840
1-417	497386.49	136154.74	55.476
1-419	497434.25	136169.90	55.725
1-420	497457.55	136175.95	55.279
1-423	497530.58	136197.47	56.268



LINE-SHOT#	EASTING	NORTHING	ELEVATION
1-425	497578.47	136211.04	56.627
1-427	497613.92	136221.15	57.106
1-429	497671.75	136246.55	57.790
1-431	497711.49	136276.66	57.934
1-434	497770.61	136323.13	58.357
1-435	497781.16	136329.98	58.335
1-436	497816.33	136342.00	57.382
1-437	497826.69	136349.15	57.315
1-438	497849.34	136359.86	56.413
1-439	497870.79	136372.00	56.403
1-445	498010.87	136442.00	52.322
1-446	498035.60	136444.88	50.855
1-447	498061.15	136448.19	50.353
1-448	498085.05	136454.86	48.903
1-451	498154.26	136474.61	44.321
1-454	498219.82	136503.79	37.921
1-455	498243.51	136499.25	37.774
1-457	498293.23	136498.23	37.773
1-459	498343.30	136494.57	37.413
1-461	498379.49	136462.94	37.653
1-463	498426.09	136460.27	39.115
1-466	498497.67	136482.41	50.565
1-467	498521.25	136490.29	53.107
1-469	498569.46	136505.18	56.331
1-471	498613.22	136527.04	58.183
1-473	498656.50	136554.00	59.606
1-475	498698.02	136580.18	59.901
1-477	498738.82	136608.08	59.323
1-479	498784.20	136638.35	58.841
1-481	498831.83	136648.94	59.328
1-482	498856.66	136654.46	59.636
1-483	498880.88	136659.89	59.463
1-484	498905.68	136665.02	58.907
1-485	498929.67	136669.47	58.148
1-486	498953.40	136672.64	57.076
1-487	498977.03	136674.46	56.380
1-488	499002.14	136674.51	55.715
1-489	499027.20	136674.35	54.523
1-490	499052.14	136674.33	53.291
1-491	499076.64	136677.47	51.746
1-492	499100.38	136682.21	50.073
1-493	499124.03	136692.59	45.798
1-494	499146.09	136700.42	41.101
1-496	499172.91	136736.83	37.390
1-497	499169.17	136754.54	37.374
1-498	499167.91	136779.36	37.506
1-502	499234.85	136869.22	37.909
1-503	499241.80	136872.72	37.854
1-505	499283.64	136902.90	38.481
1-507	499317.10	136901.28	40.065
1-511	499398.92	136873.55	46.550
1-512	499424.07	136867.87	47.261
1-513	499447.63	136862.51	46.731
1-514	499476.08	136863.63	47.255
1-515	499499.52	136867.31	47.335
1-517	499550.12	136871.95	48.662
1-518	499574.65	136871.48	49.057
1-519	499599.07	136873.61	49.406
1-520	499622.66	136877.39	49.823
1-521	499643.08	136888.89	49.790
1-522	499658.92	136907.25	49.261
1-523	499679.22	136917.99	48.905
1-524	499703.10	136929.77	49.387
1-525	499722.57	136940.52	50.647
1-526	499747.74	136949.63	53.202
1-527	499771.65	136953.79	54.387
1-528	499796.45	136958.16	54.742
1-529	499820.59	136962.33	54.559
1-531	499870.17	136971.16	54.309
1-532	499894.72	136975.61	54.850
1-533	499918.92	136980.21	55.714



LINE-SHOT#	EASTING	NORTHING	ELEVATION
1-534	499943.72	136984.35	56.403
1-535	499968.50	136988.86	56.917
2-101	491580.23	140006.89	72.186
2-102	491585.72	139995.65	72.604
2-103	491593.49	139958.84	73.691
2-104	491599.89	139935.06	74.476
2-105	491605.26	139910.45	75.310
2-106	491611.17	139886.80	76.365
2-107	491617.83	139862.74	77.577
2-108	491624.50	139838.37	78.914
2-109	491633.44	139815.29	80.267
2-110	491643.29	139792.72	81.884
2-111	491651.52	139769.71	84.328
2-112	491655.47	139745.67	87.133
2-113	491652.82	139721.69	89.210
2-114	491646.30	139697.65	90.720
2-115	491640.99	139673.72	91.398
2-116	491605.03	139657.14	92.132
2-117	491591.77	139655.60	91.729
2-118	491581.20	139649.86	91.251
2-120	491558.13	139599.75	88.232
2-121	491560.55	139576.04	88.584
2-122	491561.83	139551.12	88.772
2-123	491561.51	139526.38	89.567
2-124	491559.69	139501.65	90.210
2-125	491557.18	139475.16	90.985
2-126	491554.25	139450.58	91.859
2-127	491551.26	139427.48	92.588
2-128	491546.33	139400.14	93.880
2-129	491543.66	139388.76	94.269
2-131	491529.35	139316.41	97.869
2-132	491527.09	139304.38	98.554
2-133	491521.30	139279.93	100.104
2-134	491516.10	139255.54	101.560
2-135	491512.50	139243.95	102.048
2-137	491497.10	139183.05	104.598
2-139	491484.68	139136.35	106.674
2-141	491469.98	139088.12	109.006
2-143	491456.26	139040.69	111.165
2-145	491445.67	138992.21	112.906
2-147	491435.81	138943.08	114.178
2-149	491426.15	138894.34	115.547
2-151	491419.47	138845.02	116.946
2-152	491416.28	138820.46	117.551
2-157	491474.02	138715.86	116.830
2-158	491476.66	138703.51	116.704
2-159	491485.66	138668.60	116.672
2-160	491488.34	138656.69	116.692
2-161	491497.28	138632.83	116.746
2-162	491508.54	138609.16	116.781
2-163	491520.93	138588.09	117.032
2-164	491532.94	138566.36	117.752
2-165	491538.51	138555.39	117.883
2-166	491551.96	138521.60	118.413
2-167	491555.61	138495.64	118.921
2-168	491566.29	138474.39	119.197
2-169	491581.56	138454.02	119.172
2-170	491588.82	138443.79	118.733
2-178	491726.59	138270.48	118.621
2-179	491748.18	138262.08	118.654
2-180	491720.24	138214.40	121.541
2-181	491724.34	138202.98	122.089
2-182	491733.07	138180.08	123.344
2-183	491747.73	138146.19	126.610
2-184	491747.73	138146.19	126.610
2-187	491771.55	138062.74	132.676
2-189	491785.16	138015.35	135.664
2-191	491788.05	137965.82	139.686
2-192	491793.41	137941.82	141.271
2-193	491801.28	137932.29	141.969
2-197	491834.32	137842.04	134.695





LINE-SHOT#	EASTING	NORTHING	ELEVATION
2-198	491826.82	137832.45	133.121
2-199	491809.34	137814.74	130.464
2-201	491768.13	137786.75	125.259
2-202	491748.20	137773.11	122.973
2-203	491740.05	137763.48	121.816
2-205	491716.36	137720.53	118.346
2-206	491713.72	137683.54	116.542
2-209	491736.00	137611.56	116.333
2-211	491749.63	137577.55	117.417
2-213	491780.19	137542.57	118.542
2-215	491790.37	137482.02	114.829
2-217	491795.40	137432.06	108.210
2-219	491801.87	137383.35	101.019
2-220	491803.74	137358.20	98.528
2-221	491804.14	137334.94	96.695
2-223	491808.15	137295.89	94.059
2-225	491825.01	137252.94	91.619
2-226	491838.53	137218.19	91.164
2-227	491844.58	137204.79	91.068
2-231	491900.95	137100.18	90.708
2-232	491886.99	137065.99	90.891
2-235	491873.64	137013.33	91.190
2-236	491855.00	136981.29	91.400
2-237	491842.46	136959.29	91.781
2-238	491836.49	136948.50	92.209
2-240	491814.53	136903.38	92.619
2-252	491845.30	136664.05	96.889
2-253	491839.30	136639.35	97.560
2-254	491836.47	136627.52	97.829
2-255	491829.18	136590.46	98.521
2-256	491824.15	136566.41	99.040
2-257	491819.23	136541.78	99.478
2-258	491814.21	136517.77	99.952
2-259	491809.17	136492.93	100.445
2-260	491804.09	136468.22	100.985
2-261	491799.04	136443.66	101.662
2-264	491796.75	136386.39	105.087
2-265	491777.27	136355.55	107.100
2-267	491753.95	136311.60	111.056
2-268	491741.61	136289.24	113.065
2-269	491735.59	136278.13	113.850
2-270	491718.09	136245.42	116.100
2-271	491712.50	136234.52	116.890
2-272	491694.98	136202.38	119.082
2-273	491688.96	136191.14	119.596
2-274	491671.77	136157.81	120.590
2-275	491666.14	136146.78	120.782
2-276	491648.27	136113.44	121.562
2-277	491642.94	136102.77	121.790
2-278	491625.54	136069.46	122.328
2-279	491614.52	136047.37	122.951
2-280	491600.54	136013.75	124.110
2-281	491596.75	136001.49	124.368
2-282	491594.06	135992.04	124.439
2-283	491582.70	135954.21	123.782
2-284	491579.10	135942.11	123.493
2-285	491572.98	135918.42	122.801
2-286	491571.83	135881.21	123.695
2-287	491575.73	135856.88	125.499
2-288	491580.16	135832.61	126.912
2-289	491584.92	135807.94	127.687
2-290	491589.45	135783.64	127.877
2-291	491594.39	135758.80	127.762
2-292	491598.81	135734.31	127.667
2-293	491602.52	135709.47	128.021
2-294	491607.15	135685.09	128.033
2-295	491611.40	135660.43	127.531
2-296	491615.44	135635.54	126.736
2-297	491617.04	135623.31	126.261
3-104	493296.71	137759.05	91.684
3-105	493302.49	137734.91	89.813



LINE-SHOT#	EASTING	NORTHING	ELEVATION
3-106	493307.84	137710.08	88.364
3-107	493311.81	137685.55	87.324
3-108	493314.82	137661.18	86.695
3-109	493317.56	137636.83	86.197
3-110	493319.08	137611.57	85.269
3-111	493320.14	137586.36	83.977
3-112	493320.96	137561.29	82.620
3-113	493322.14	137536.69	81.555
3-114	493323.42	137499.10	80.332
3-115	493323.76	137487.23	79.989
3-116	493319.16	137465.14	79.283
3-117	493305.71	137437.11	78.008
3-118	493297.15	137418.09	76.734
3-119	493292.88	137408.56	76.118
3-120	493277.27	137370.09	71.826
3-121	493273.94	137347.02	68.498
3-122	493272.22	137334.57	66.913
3-123	493268.04	137285.41	69.279
3-124	493266.21	137274.17	71.749
3-125	493265.48	137261.26	73.662
3-126	493268.92	137211.65	77.384
3-127	493269.76	137200.61	77.810
3-128	493271.29	137175.43	78.594
3-129	493272.44	137149.29	79.020
3-130	493273.65	137124.82	79.052
3-131	493274.67	137099.57	79.065
3-132	493275.76	137074.57	79.326
3-133	493276.87	137050.43	79.541
3-134	493277.84	137025.01	79.770
3-135	493278.85	137000.00	79.839
3-136	493280.08	136976.12	80.011
3-137	493280.97	136952.64	80.456
3-139	493280.56	136887.54	80.717
3-141	493261.97	136856.16	80.661
3-142	493253.89	136832.01	79.626
3-143	493253.73	136818.76	78.730
3-148	493313.76	136701.61	77.349
3-149	493304.86	136693.79	78.309
3-150	493296.48	136684.25	79.420
3-151	493269.34	136658.33	79.725
3-152	493260.70	136649.52	79.616
3-153	493245.97	136629.89	79.568
3-155	493207.02	136566.06	80.219
3-157	493197.48	136543.07	80.592
3-158	493189.91	136506.17	81.122
3-161	493187.14	136444.85	83.315
3-163	493194.82	136381.76	84.572
3-164	493200.03	136355.56	84.951
3-165	493201.47	136346.37	85.155
3-169	493232.08	136212.70	86.373
3-171	493240.18	136164.84	86.855
3-173	493249.05	136114.47	86.217
3-175	493257.59	136065.19	84.903
3-177	493266.01	136015.59	83.781
3-179	493272.34	135980.30	82.902
3-180	493268.86	135953.90	82.517
3-181	493259.01	135931.06	81.721
3-182	493241.63	135896.60	81.018
3-183	493233.33	135888.42	80.810
3-185	493199.54	135840.81	82.200
3-187	493189.77	135791.88	81.765
3-189	493165.04	135750.56	82.253
3-191	493147.24	135705.44	83.431
3-193	493139.13	135655.72	82.351
3-194	493135.91	135631.31	81.735
3-195	493133.01	135619.36	81.504
3-199	493212.59	135566.99	76.379
3-200	493226.31	135547.17	85.017
3-200A	493217.82	135538.60	85.433
3-201	493200.46	135520.57	85.886
3-202	493185.98	135501.49	87.781



LINE-SHOT#	EASTING	NORTHING	ELEVATION
3-205	493168.00	135429.92	90.763
3-207	493165.09	135379.84	89.822
3-209	493161.20	135331.45	87.821
3-211	493166.07	135281.31	88.808
3-213	493152.36	135233.84	90.990
3-215	493137.11	135200.20	90.216
3-217	493194.18	135176.20	99.488
3-218	493217.13	135173.84	105.702
3-219	493239.24	135168.84	109.446
3-220	493251.32	135163.88	110.313
3-226	493420.01	135067.94	106.688
3-227	493416.62	135042.70	105.278
3-231	493315.07	134956.18	106.510
3-232	493310.22	134945.93	105.915
3-233	493299.29	134922.47	104.701
3-235	493278.36	134876.73	102.425
3-237	493257.54	134832.19	99.779
3-239	493236.96	134787.32	98.472
3-240	493231.59	134774.98	98.335
3-241	493203.21	134751.52	98.409
3-242	493181.84	134739.72	98.025
3-243	493160.51	134725.70	97.154
3-244	493143.64	134708.57	96.134
3-245	493132.62	134691.11	95.558
3-246	493130.36	134665.77	94.517
3-247	493130.79	134641.41	94.086
3-248	493133.59	134616.68	92.996
3-249	493132.88	134590.40	92.193
3-250	493146.12	134576.63	91.394
3-251	493178.21	134560.31	90.807
3-252	493185.11	134549.46	90.266
3-253	493198.37	134527.04	89.935
3-254	493210.78	134503.34	90.460
3-255	493221.70	134480.60	90.883
3-256	493233.10	134457.69	91.311
3-257	493243.16	134438.06	91.090
3-258	493255.35	134414.05	91.096
3-259	493265.02	134392.92	90.790
3-260	493275.34	134369.39	90.025
3-261	493279.67	134358.55	89.811
3-262	493267.86	134323.04	88.505
3-263	493256.59	134318.07	87.905
3-264	493207.03	134313.37	84.659
3-265	493161.01	134310.12	81.488
3-266	493109.79	134336.14	79.879
3-268	493169.48	134200.78	73.049
3-269	493160.21	134191.43	73.097
3-270	493143.33	134174.64	72.798
3-271	493120.39	134157.62	72.186
3-272	493109.85	134157.36	72.479
4-101	494659.22	132465.14	101.462
4-102	494677.46	132497.45	101.043
4-103	494683.61	132508.23	100.754
4-104	494696.96	132529.90	99.666
4-105	494708.61	132552.14	97.796
4-106	494720.12	132573.31	95.847
4-107	494732.52	132594.87	93.811
4-108	494745.13	132616.45	91.917
4-109	494757.61	132638.13	90.334
4-110	494770.02	132659.40	89.058
4-111	494782.26	132680.69	87.724
4-112	494794.57	132702.20	86.259
4-113	494807.20	132723.65	85.082
4-114	494819.43	132745.08	84.125
4-115	494831.56	132766.59	83.150
4-116	494843.95	132787.93	82.354
4-117	494856.38	132809.32	81.567
4-118	494869.16	132831.45	80.940
4-119	494881.13	132852.14	80.429
4-120	494896.14	132871.68	79.755
4-121	494915.50	132905.34	78.578



LINE-SHOT#	EASTING	NORTHING	ELEVATION
4-122	494921.55	132916.31	78.241
4-123	494938.79	132947.21	77.309
4-124	494945.51	132959.50	77.002
4-131	495006.75	133123.22	75.873
4-132	495014.75	133145.73	76.130
4-133	495023.52	133169.15	75.982
4-134	495033.37	133192.74	75.734
4-136	495060.17	133247.85	75.523
4-137	495065.73	133258.44	75.499
4-138	495077.76	133280.40	75.630
4-139	495083.76	133291.33	75.755
4-142	495095.22	133390.16	75.677
4-143	495103.59	133404.38	75.630
4-144	495118.23	133426.41	75.777
4-145	495130.08	133449.58	75.965
4-146	495149.66	133468.10	76.094
4-147	495164.84	133487.79	76.488
4-148	495178.03	133510.10	76.862
4-149	495191.23	133532.40	77.237
4-150	495203.10	133552.59	77.064
4-151	495212.68	133575.11	77.203
4-152	495222.67	133596.11	77.190
4-153	495232.13	133616.50	77.110
4-154	495239.38	133637.79	77.244
4-169	495360.26	133995.26	80.560
4-170	495369.79	134003.83	80.186
4-171	495385.93	134021.50	79.471
4-172	495402.64	134039.95	78.710
4-173	495418.26	134057.30	77.657
4-174	495434.30	134075.45	76.438
4-175	495442.68	134084.86	75.827
4-177	495463.91	134140.75	73.233
4-179	495483.65	134186.22	71.667
4-181	495499.22	134228.96	71.404
4-183	495471.06	134269.93	71.997
4-185	495440.79	134309.88	70.733
4-187	495410.52	134349.75	69.555
4-189	495415.24	134395.80	67.384
4-191	495425.24	134443.73	66.081
4-193	495438.28	134492.48	65.039
4-195	495452.74	134540.50	64.272
4-197	495476.35	134583.76	64.125
4-199	495500.00	134627.10	64.381
4-201	495503.34	134675.65	64.821
4-202	495500.90	134700.20	63.215
4-206	495492.22	134789.56	53.879
4-208	495499.63	134838.98	50.798
4-209	495492.69	134861.78	50.863
4-211	495472.56	134906.50	60.120
4-213	495465.08	134953.82	63.661
4-215	495460.18	135002.39	64.317
4-216	495430.34	134995.29	66.423
4-217	495417.03	135017.12	66.186
4-218	495409.27	135039.89	67.061
4-219	495401.50	135063.60	67.695
4-224	495332.50	135161.83	59.414
4-225	495310.64	135173.65	59.083
4-226	495288.78	135185.47	58.751
4-236	495191.88	135359.42	72.745
4-237	495181.03	135381.40	76.205
4-238	495175.19	135405.62	79.298
4-239	495169.43	135429.36	81.982
4-241	495145.15	135469.30	85.040
4-243	495095.82	135475.75	85.208
4-244	495076.25	135488.29	85.935
4-245	495068.42	135511.25	86.680
4-246	495065.82	135535.92	86.426
4-247	495063.22	135560.59	86.171
4-250	495076.77	135633.08	79.621
4-251	495082.44	135657.14	78.326
4-259	494977.93	135785.71	76.675



LINE-SHOT#	EASTING	NORTHING	ELEVATION
4-260	494965.81	135806.40	75.198
4-261	494953.18	135828.23	73.540
4-262	494948.91	135853.72	71.978
4-268	494872.31	135966.17	68.288
4-269	494884.31	135962.39	68.519
4-270	494906.35	135965.23	68.405
4-271	494925.31	135980.97	68.869
4-273	494951.82	136008.20	68.615
4-275	494987.86	136056.74	69.030
4-277	494993.26	136102.58	72.227
4-279	494978.15	136135.66	74.160
4-281	494958.89	136190.62	74.659
4-283	494964.56	136240.40	73.993
4-285	495000.22	136253.69	73.174
4-287	495046.22	136271.95	72.203
4-289	495092.42	136283.45	70.717
4-290	495105.81	136280.98	70.331
4-294	495078.52	136392.82	62.360
4-295	495136.19	136400.57	69.164
4-297	495183.23	136405.80	68.038
4-299	495204.13	136452.61	67.374
4-301	495221.59	136498.20	66.268
4-303	495234.10	136546.06	65.706
4-304	495233.50	136570.38	63.979
4-305	495249.42	136590.47	63.477
4-306	495266.97	136608.55	63.823
4-307	495282.91	136625.36	64.230
4-308	495296.27	136647.92	64.374
4-309	495300.58	136673.17	64.982
4-310	495290.77	136695.03	66.825
4-311	495252.86	136686.28	67.931
4-314	495273.64	136773.68	50.367
4-315	495236.37	136798.66	50.402
4-316	495242.16	136809.20	50.816
4-317	495239.99	136853.87	63.141
4-318	495238.69	136865.37	64.343
4-319	495235.68	136890.11	66.278
4-320	495232.83	136915.30	67.323
4-321	495229.91	136940.17	68.098
4-322	495228.32	136951.18	68.198
4-330	495244.22	137169.72	63.941
4-331	495245.38	137181.94	63.888
4-332	495244.50	137207.55	63.933
4-333	495246.76	137232.03	64.289
4-334	495254.21	137255.49	64.999
4-335	495256.61	137279.14	65.499
4-336	495257.64	137290.44	65.733
4-339	495249.09	137376.21	66.466
4-340	495246.83	137402.53	66.592
4-341	495244.82	137427.97	66.902
4-342	495242.57	137452.51	67.299
4-343	495239.47	137476.84	67.738
4-344	495235.31	137502.76	67.685
4-345	495231.40	137513.92	67.612
4-347	495225.28	137562.05	66.947
4-348	495228.30	137611.14	67.185
4-349	495230.93	137622.70	68.211
4-350	495236.20	137647.27	68.989
4-351	495241.04	137671.46	69.723
4-352	495246.66	137697.00	70.080
4-353	495252.09	137721.61	70.448
4-354	495256.89	137744.86	70.678
4-355	495260.00	137770.55	71.365
4-357	495285.46	137817.46	71.959
4-358	495295.94	137824.64	72.421
4-359	495317.18	137839.79	73.150
4-360	495326.30	137845.68	73.506
5-101	490783.42	135687.64	192.255
5-102	490798.49	135705.83	191.530
5-103	490814.75	135726.17	190.240
5-104	490829.09	135746.72	187.912



LINE-SHOT#	EASTING	NORTHING	ELEVATION
5-105	490839.22	135769.12	185.083
5-106	490846.08	135793.36	183.901
5-107	490849.46	135817.97	183.101
5-108	490853.74	135842.08	180.883
5-109	490876.99	135870.96	179.168
5-110	490897.36	135889.81	177.238
5-111	490916.42	135912.78	175.735
5-112	490932.81	135940.06	174.592
5-113	490969.69	135849.68	163.619
5-114	490992.32	135858.89	160.873
5-115	491015.30	135868.32	157.880
5-116	491036.87	135878.23	153.645
5-117	491060.18	135887.72	149.994
5-118	491071.76	135892.09	148.929
5-120	491126.30	135886.99	144.614
5-121	491150.64	135891.71	142.630
5-122	491174.59	135897.01	141.284
5-123	491199.17	135900.71	140.742
5-124	491223.67	135898.36	141.109
5-125	491247.69	135903.68	140.045
5-126	491268.60	135908.16	138.812
5-127	491278.25	135917.91	138.236
5-128	491305.34	135920.74	136.739
5-129	491327.34	135915.36	135.404
5-130	491353.24	135917.82	134.708
5-131	491377.17	135917.77	133.286
5-132	491403.86	135921.15	132.080
5-133	491425.93	135925.48	130.898
5-135	491475.92	135931.21	128.169
5-137	491525.00	135929.20	125.798
5-139	491573.96	135926.65	122.932
5-141	491589.90	135981.09	124.430
5-143	491607.67	136033.45	123.559
5-145	491631.91	136082.45	122.179
5-147	491656.41	136129.57	121.244
5-149	491680.95	136176.82	120.150
5-151	491705.77	136222.99	117.686
5-153	491731.29	136271.54	114.291
5-155	491758.38	136320.70	109.999
5-157	491785.75	136369.71	106.391
5-159	491905.46	136300.88	107.669
5-161	491947.70	136330.87	104.802
5-163	491986.02	136357.35	102.893
5-165	492035.45	136355.37	100.998
5-167	492085.80	136361.88	98.794
5-169	492106.65	136392.71	97.973
5-171	492134.39	136433.38	96.899
5-173	492148.18	136481.67	95.837
5-175	492158.25	136517.69	95.203
5-179	492261.35	136530.29	99.313
5-181	492308.97	136544.45	100.625
5-182	492328.17	136559.54	100.336
5-183	492346.28	136574.92	99.695
5-185	492384.09	136610.81	98.904
5-187	492420.26	136645.95	97.972
5-188	492437.92	136663.21	97.447
5-189	492455.12	136680.94	97.049
5-191	492486.94	136719.91	95.886
5-193	492517.48	136759.11	95.197
5-195	492550.84	136796.54	94.227
5-198	492602.07	136850.82	93.054
5-199	492618.58	136870.60	92.549
5-201	492648.77	136909.00	91.476
5-203	492678.48	136950.05	90.152
5-205	492711.62	136985.55	89.034
5-207	492805.02	136953.63	88.016
5-208	492859.16	136933.89	88.920
5-210	492894.53	136970.22	87.430
5-211	492897.41	136999.94	85.930
5-213	492904.56	137072.59	83.137
5-215	492910.98	137136.14	81.682



LINE-SHOT#	EASTING	NORTHING	ELEVATION
5-216	492914.57	137168.15	81.234
5-219	492977.68	137185.23	79.745
5-221	493035.04	137208.16	79.234
5-223	493079.32	137230.64	78.559
5-225	493118.72	137262.26	77.875
5-226	493136.60	137279.44	77.748
5-227	493135.15	137304.30	78.257
5-228	493133.23	137316.48	77.867
5-229	493169.40	137329.61	76.054
5-230	493180.50	137350.89	71.612
5-231	493200.03	137363.04	68.581
5-232	493222.93	137361.81	65.633
5-234	493259.23	137383.38	70.699
5-235	493283.17	137415.29	76.206
5-236	493295.25	137409.93	76.233
5-237	493317.04	137401.07	75.819
5-238	493341.65	137394.58	76.292
5-239	493361.58	137411.28	77.152
5-240	493376.04	137430.96	76.747
5-241	493390.38	137451.12	77.179
5-242	493404.71	137471.27	77.612
5-243	493413.73	137494.01	78.658
5-244	493416.73	137507.13	79.208
5-245	493448.61	137526.35	79.689
5-246	493468.78	137540.90	79.892
5-247	493486.37	137559.74	80.415
5-248	493500.47	137580.29	81.105
5-249	493512.06	137602.82	81.789
5-250	493521.04	137625.79	82.377
5-251	493536.34	137644.47	83.486
5-252	493557.14	137658.25	83.982
5-253	493567.68	137665.30	84.268
5-254	493588.30	137679.33	84.698
5-256	493639.61	137713.54	86.608
5-257	493660.91	137727.56	88.278
5-258	493671.52	137734.60	88.818
5-260	493712.80	137762.55	90.253



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## APPENDIX C. BIBLIOGRAPHY AND REFERENCES

Oxford Archaeology, 2009, Land Adjacent to Oldbury Power Station: Shepperdine, South Gloucestershire. Archaeological Evaluation Report (Unpublished Client Report available from the HER).

## APPENDIX D. SUMMARY OF SITE DETAILS

**Site name:** Godley Bridge Survey, Surrey  
**Site code:** CHGOB 10  
**Grid reference:** SU 93450 37670 and SU 93142 36096  
**Type:** Evaluation  
**Date and duration:** 26th May 2010  
**Area of site:** Two trial pits 2.5 m-3.5 m by 1.5 m.

### Summary of results:

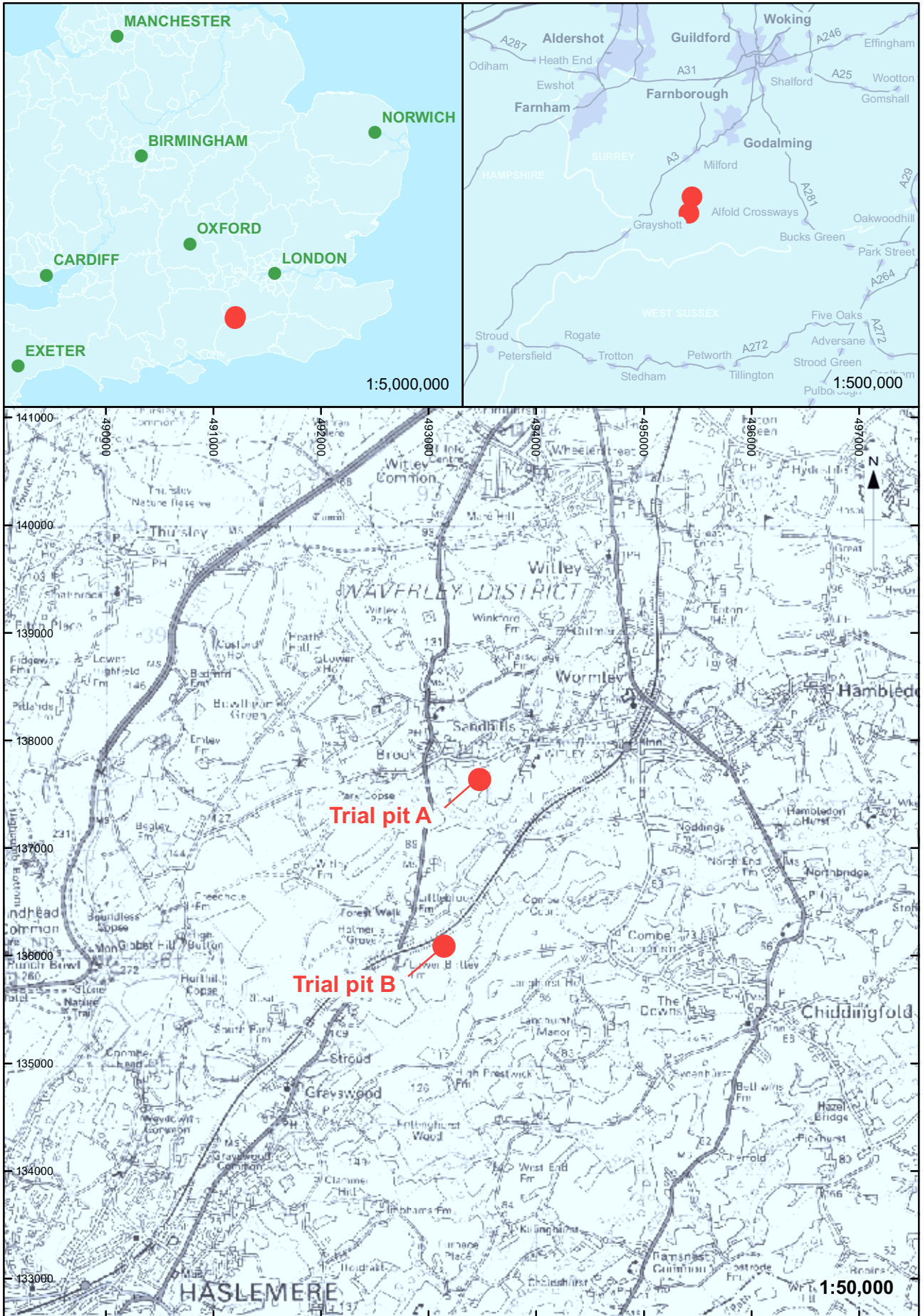
On 26th May 2010 Oxford Archaeology undertook a field impact assessment of geotechnical seismic survey investigations on the potential archaeological resource at two trial locations north-east of Haslemere, Surrey. The investigation was undertaken in advance of, and to inform, a programme of geotechnical prospecting within the surrounding landscape.

The survey utilised a 200g explosive charge buried 2 m deep into the underlying sediments. Controlled archaeological excavation and sampling of the discharged explosive locations established that these had a localised impact on the surrounding sediment that is unlikely to significantly affect archaeological remains. The explosive force created blast craters with diameters of c 0.65 m surrounded by areas of sediment compaction. The localised outcrops of ironstone found within the Weald Clay Formation were found to be resilient to the impacts of the blast. As would be expected, in comparison with similar studies on softer alluvial sediments (alluvial clays), the impact of the blast was found to be proportionally less on harder bedrock sediments.

### Location of archive:

The archive is currently held at OA, Janus House, Osney Mead, Oxford, OX2 0ES. This will be deposited with a local receiving museum in due course. Currently Guildford Museum deferred to Godalming Museum which has been contacted but has not replied to this request.





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Figure 1: Site location



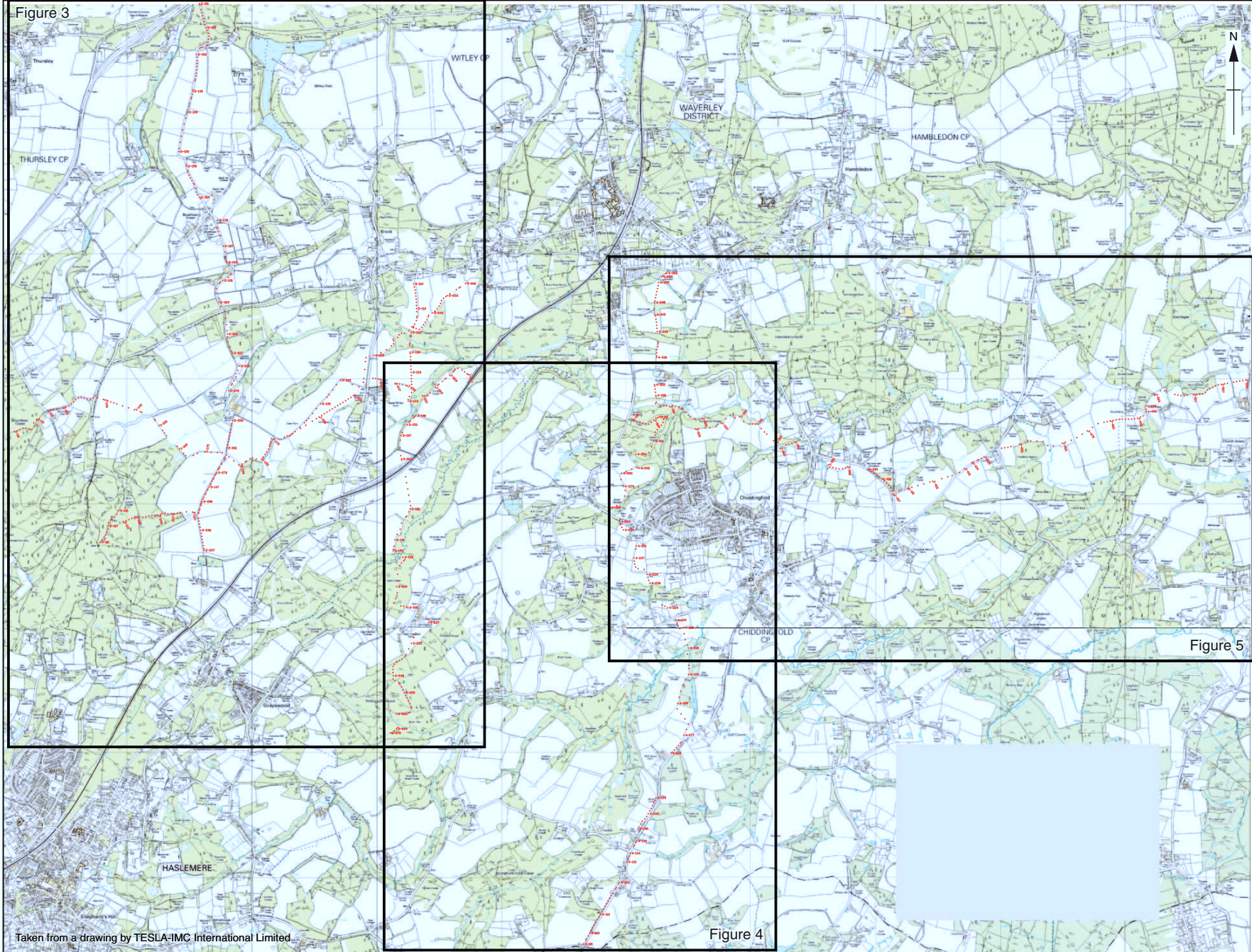
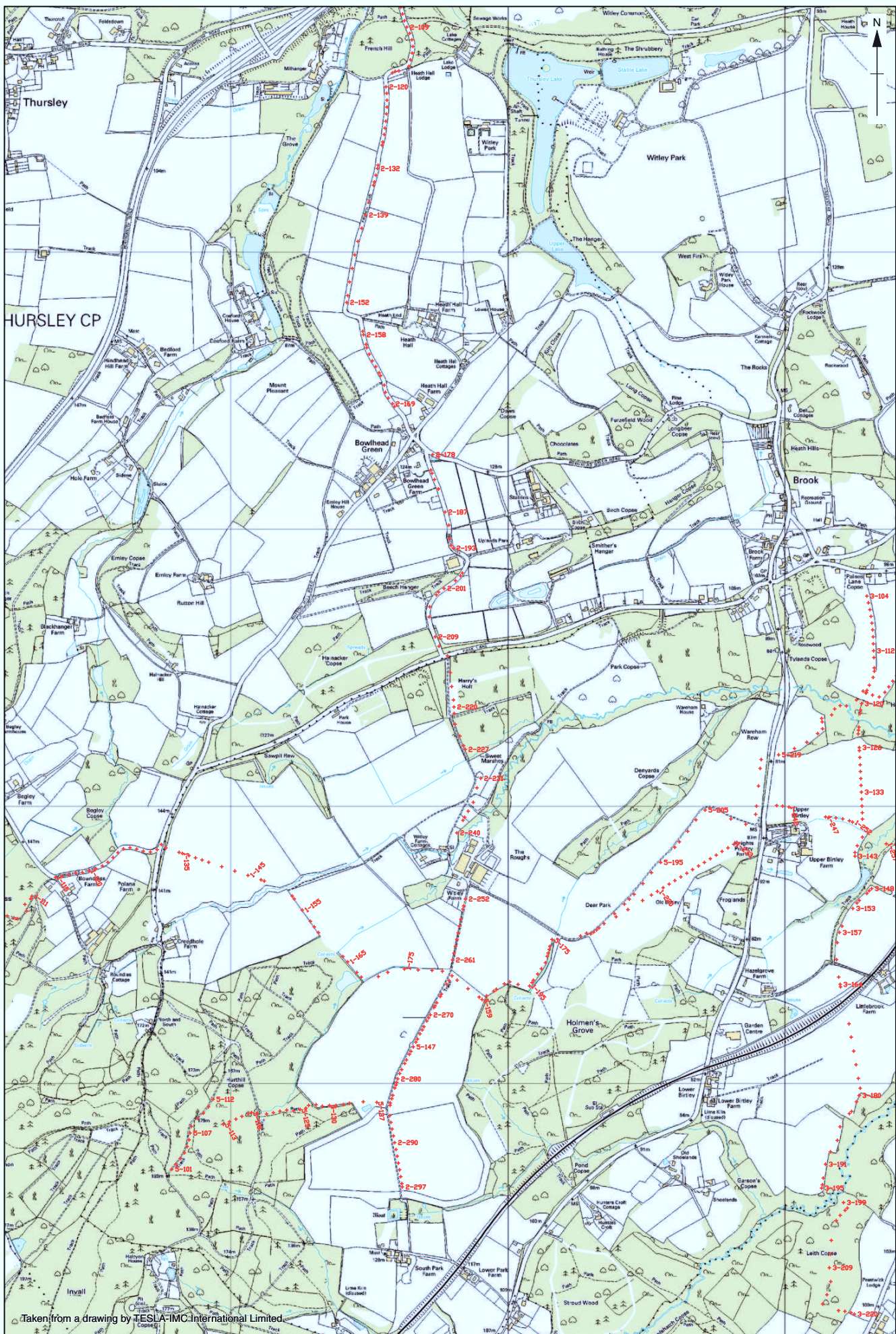


Figure 2

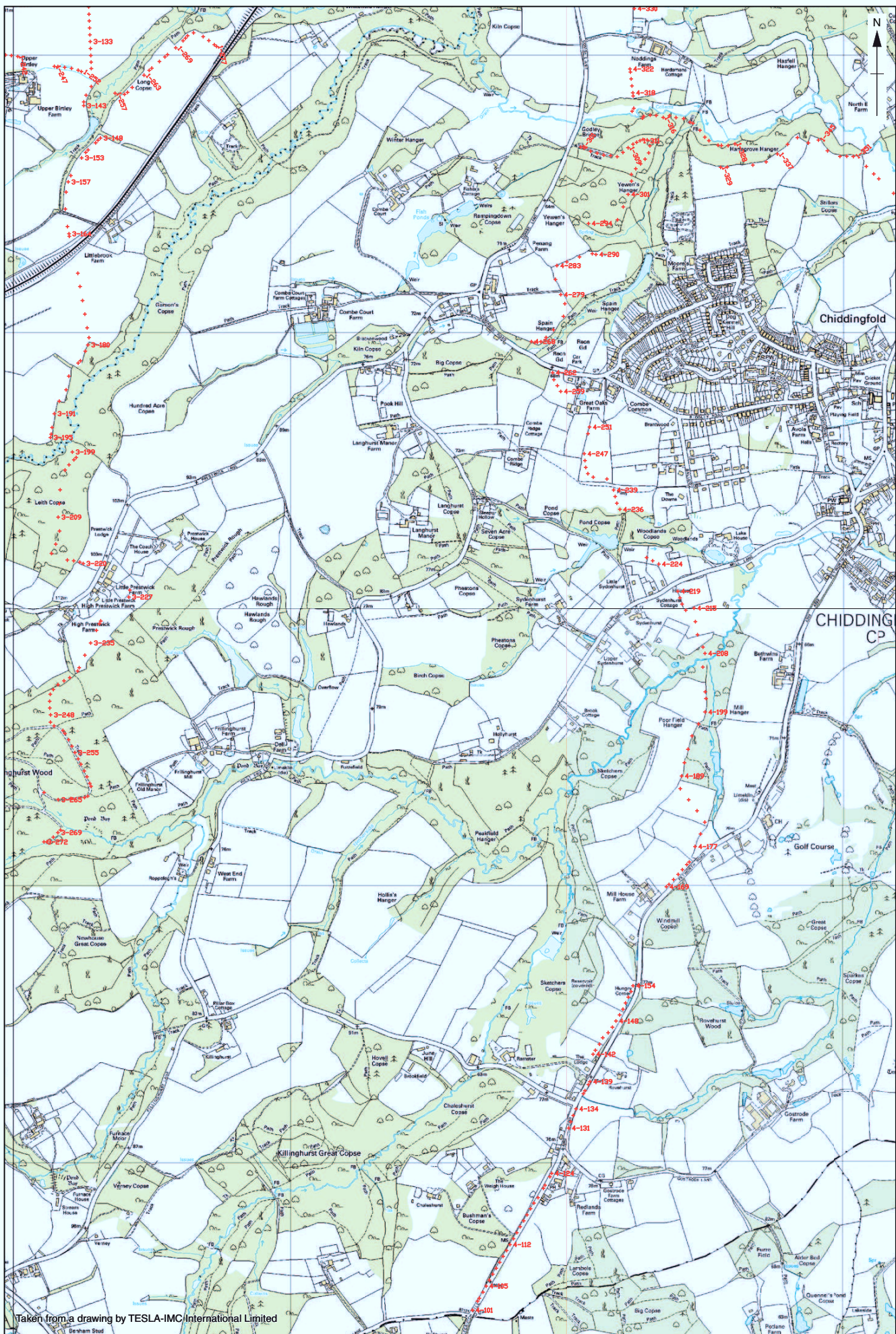




Taken from a drawing by TESLA-IMC International Limited

Figure 3





Taken from a drawing by TESLA-IMC International Limited

Figure 4





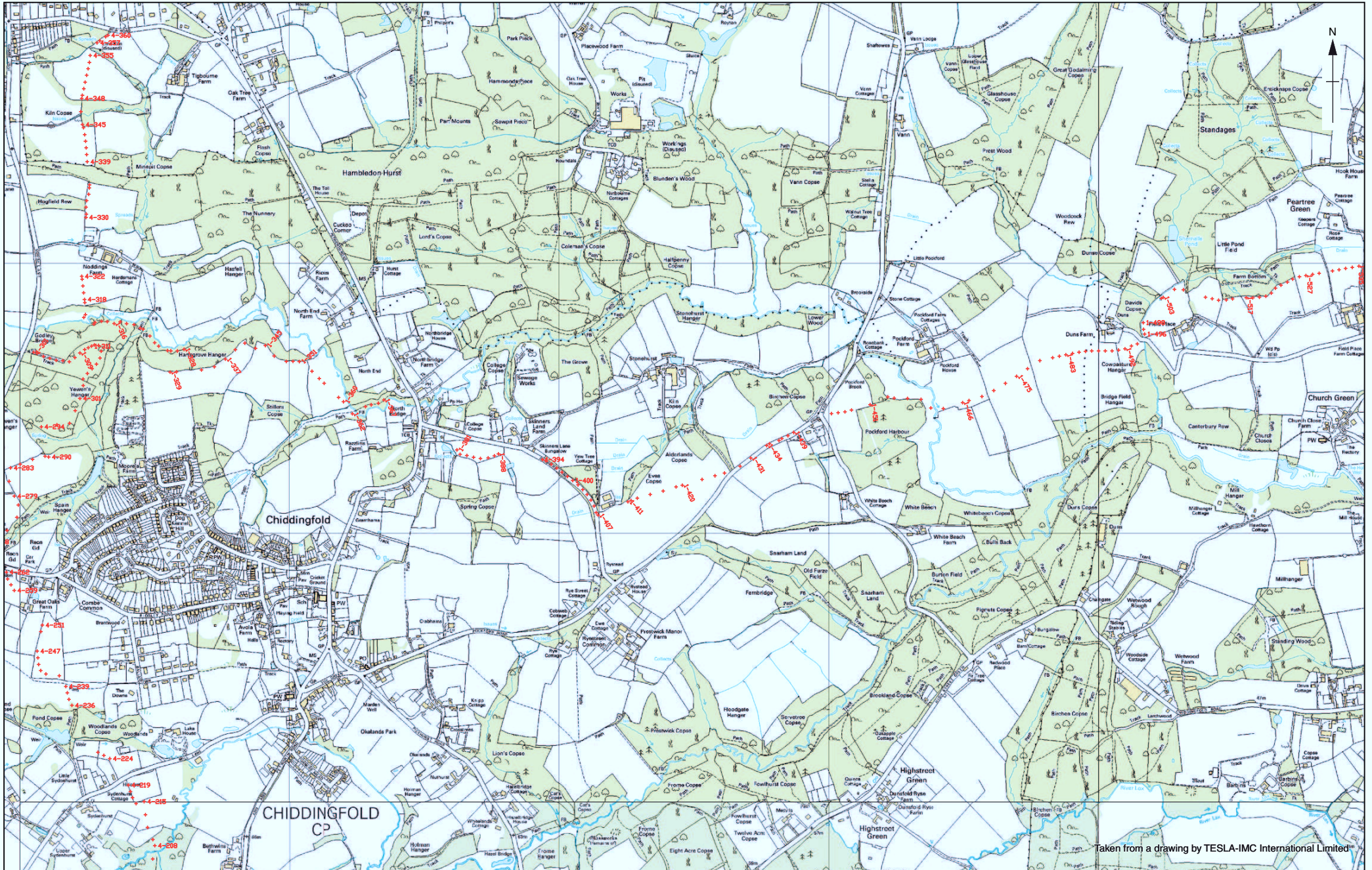


Figure 5



## Plates



Plate 1: Auger drilling to a depth of 2m in preparation for the seismic charge at TP1



Plate 2: Section of Trial Pit 1 showing the blast crater of a 200g explosive charge





Plate 3: Auger drilling at location TP2 in preparation for the seismic charge



Plate 4: Section of Trial Pit 2 showing the blast crater of a 200g explosive charge





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